

Approximate Analysis of Power Offset over Spatially Correlated MIMO Channels

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Abstract: Power offset is zero-order term in the capacity versus signal-to-noise ratio curve. In this paper, approximate analysis of power offset is presented to describe MIMO system with uniform linear antenna arrays of fixed length. It is assumed that the number of receive antenna is larger than that of transmit antenna. Spatially Correlated MIMO Channel is approximated by tri-diagonal toeplitz matrix. The determinant of tri-diagonal toeplitz matrix, which is fitted by elementary curve, is one of the key factors related to power offset. Based on the curve fitting, the determinant of tri-diagonal toeplitz matrix is mathematically tractable. Consequently, the expression of local extreme points can be derived to optimize power offset. The simulation results show that approximation above is accurate in local extreme points of power offset. The proposed expression of local extreme points is helpful to approach optimal power offset.

Keywords: MIMO, multiplexing gain, power offset, high snr region, toeplitz matrix

1. Introduction

Multiple-input multiple-output (MIMO) system is widely used in wireless communication to improve the performance. The spectral efficiency of MIMO channel is much higher than that over the conventional signal antenna channel. The research of MIMO includes two different perspectives: the first one concerns performance analysis in terms of error performance of practical systems, the second one concerns the study of channel capacity.

The design of communication schemes was mainly considered in the former perspectives with the aid of theoretical analysis and simulation [1][2], and [3]. For the latter, important parameters such as diversity gain [4], multiplexing gain [5][6] (referred to degree of freedom in other literatures), and power offset [7-9], and [10] were emphatically analyzed in the high signal-to-noise ratio (SNR) region. Furthermore, diversity and multiplexing tradeoff has been proposed in [11][12], and [13], that is to say diversity and multiplexing tradeoff can be obtained for a given multiple antenna channel. It is worth pointing out in [11] that the diversity and multiplexing tradeoff is essentially the tradeoff between the error probability and the data rate of a given system.

The multiplexing gain is not sufficient to accurately characterize the property of MIMO capacity. A more accurate representation of high SNR behavior in SNR-capacity curve is provided by an affine approximation to capacity, which includes both the multiplexing gain (i.e. slope) and power offset (i.e. zero-order term) [7]. High SNR power offset has been analyzed in [8] over multiple antenna Ricean channels. It was shown in [8] that the im-

part of the Ricean factor at high SNR region could be conveniently quantified through the corresponding power offset. In [9], high SNR power offset in multiple antenna communication was derived in detail. Achievable throughput was compared between the optimal strategy of dirty paper coding and suboptimal linear precoding techniques (zero-forcing and block diagonalization) in [10] on application of power offset. Hence, power offset is an important parameter in multiple antenna communication.

In many practical environments, signal correlation among the antenna array exists due to the scattering. Fading correlation and its effect on the capacity of multielement antenna system has been studied in [14]. Hence, analysis of spatially correlated MIMO channels has been another topic in the past few years, which necessitates the model of correlated channel. A general space-time correlation model for MIMO systems in mobile fading channel has been presented in [15]. The model in [15] was flexible and mathematically tractable. In [16], the correlated model of [15] has been used to investigate the capacity of spatially correlated MIMO Rayleigh-fading channels.

Recently, application of different antenna arrays in MIMO system has also been exploited. With the consideration of physical constraints imposed by maximum size of the antenna array, uniform linear array of fixed length has been used in [17] to analyze the asymptotic capacity of MIMO systems.

The uniform linear array of fixed length is also used in this paper to analyze the power offset of MIMO system over spatially correlated channel. On application of curve fitting, the determinant of tri-diagonal toeplitz matrix is mathematically tractable. Over spatially correlated chan-

nel, the main result of this paper is the derived expression of local extreme points of power offset, using the uniform linear array of fixed length. To the best of our knowledge, the main result has not been presented in other literatures.

The rest parts are organized as follows. In Section 2, the basic definitions of multiplexing gain and power offset are presented. System model and correlation model are given in Section 3. Approximate analysis of power offset by fitting determinant curve of tri-diagonal toeplitz matrix is put forward in Section 4. Section 5 shows the simulation results. Finally, a brief conclusion is given in Section 6.

Notation: In the following context, matrices and vectors are denoted by boldface upper case symbols and boldface lower case symbols, respectively. The transpose and Hermitian transpose are denoted by $(\cdot)^T$ and $(\cdot)^H$, respectively. The expected value is represented by $E[\cdot]$. $\|\cdot\|$ is used for the Euclidian norm.

2. Basic Definition

In the high SNR region, the capacity of single-user MIMO system of coherent reception is given by [18][19]

$$C(SNR) = \min(n_T, n_R) \log_2 SNR + o(1) \quad (1)$$

where n_T, n_R denote the number of transmit and receive antenna elements, respectively. SNR is the signal to noise ratio. The MIMO capacity in high SNR region is a linear function of $\min(n_T, n_R)$, i.e. the stationary slope in SNR-capacity curve. In other words, any increase in $\max(n_T, n_R)$ is immaterial, i.e. without any impact to the slope. The slope is the so-called maximum multiplexing gain (degree of freedom).

If n_T is fixed to a given value (generally speaking, n_T is less than six, expressed as \widehat{n}_T in the following context), and $n_R \geq n_T$, the multiplexing gain equals to a fixed value without consideration of correlation of channel response and the number of receive antenna elements. So power offset is introduced to compare the impact of channel property with the same value of multiplexing gain, and (1) is replaced by [9]

$$\begin{aligned} C(SNR) &= S_\infty (\log_2(SNR) - L_\infty) + o(1) \\ &= S_\infty \left(\frac{SNR_{dB}}{3dB} - L_\infty \right) + o(1) \end{aligned} \quad (2)$$

where S_∞ is multiplexing gain and L_∞ is power offset in 3-dB units. When $SNR \rightarrow \infty$, the multiplexing gain and power offset can be computed by

$$S_\infty = \lim_{SNR \rightarrow \infty} \frac{C(SNR)}{\log_2(SNR)} \quad (3)$$

$$L_\infty = \lim_{SNR \rightarrow \infty} \left(\log_2(SNR) - \frac{C(SNR)}{S_\infty} \right) \quad (4)$$

In the high SNR region, SNR-capacity curve is approximately determined by multiplexing gain and power offset. Most channels, having the same multiplexing gain, may have very different capacities because of various values of the power offset. Hence, power offset is an important parameter to describe the capacity behavior in high SNR region.

3. System Model and Correlation Mode

The system model and channel correlation model are defined in this section. For MIMO system, the general baseband model is given by

$$\mathbf{y} = \mathbf{H}\mathbf{x} + \mathbf{n} \quad (5)$$

where \mathbf{H} is the channel response matrix, and $\mathbf{x} = [x_1 \ x_2 \ \dots \ x_{\widehat{n}_T}]^T$ is the input complex signal vector whose spatial covariance matrix normalized by the energy per dimension can be expressed as

$$\Phi = \frac{E(\mathbf{x}\mathbf{x}^H)}{\frac{1}{\widehat{n}_T} \times E[\|\mathbf{x}\|^2]} \quad (6)$$

while $\mathbf{y} = [y_1 \ y_2 \ \dots \ y_{n_R}]^T$ and $\mathbf{n} = [n_1 \ n_2 \ \dots \ n_{n_R}]^T$ are the output vector and additive white Gaussian noise vector, respectively. Because of normalization and assumption of isotropic input, $tr(\Phi) = \widehat{n}_T$ and $\Phi = \mathbf{I}_{\widehat{n}_T}$, where \mathbf{I}_n is $n \times n$ identity matrix.

Kronecker model [16] is used to describe the correlation of channel response. On the assumption of rich scattering environments and having no line of sight, the correlated channel response matrix is denoted by

$$\Sigma_H = \Sigma_T \otimes \Sigma_R \quad (7)$$

where \otimes is Kronecker product, Σ_T and Σ_R are correlated matrix of transmit and receive antenna, respectively. So the channel response matrix \mathbf{H}_Σ is given by

$$\mathbf{H}_\Sigma = \Sigma_R^{1/2} \mathbf{H} \Sigma_T^{1/2} \quad (8)$$

where \mathbf{H} is channel response matrix whose elements are independent and identical distribution random variables. Without loss of generality, we assume that the distance between transmit antenna elements is large enough to neglect the correlation at the transmit node. Consequently, without considering the antenna correlation at the transmit node, the correlation matrix Σ_T is identity matrix, and the receive antenna correlation model Σ_R is given by [15][16].

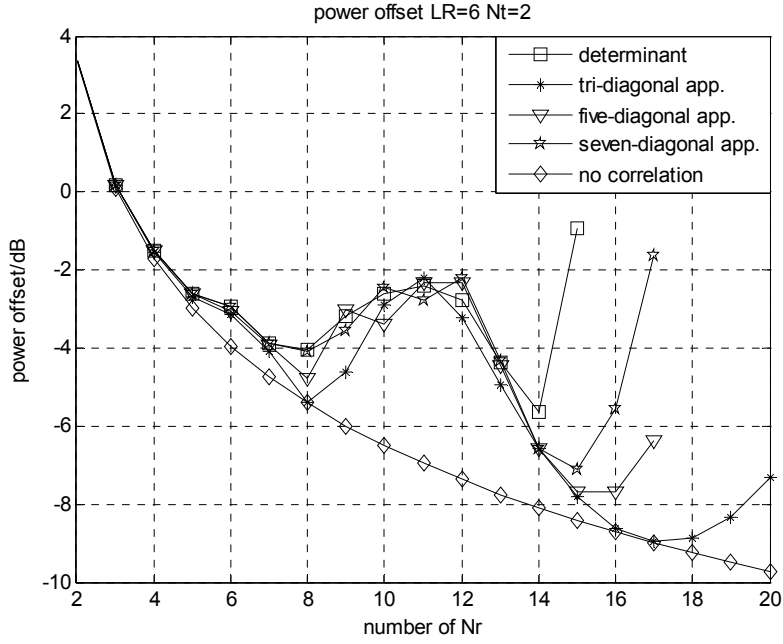


Figure 2. Approximate analysis of power offset based on 3, 5, and 7 diagonal toeplitz matrix with $L_R = 6$, $\hat{n}_T = 2$

where Λ_T and Λ_R are diagonal matrix whose elements are eigenvalues of Σ_T and Σ_R , respectively. \mathbf{P} is also diagonal matrix whose elements are eigenvalues of normalized spatial covariance matrix Φ , so \mathbf{P} is identity matrix and $1/\hat{n}_T \log_2 \det(\Lambda_T \mathbf{P})$ is constant zero. Λ_R can be derived from (11). It is obvious that Λ_R is full rank matrix, and then (13) is simplified to

$$L_\infty = \log_2 \hat{n}_T + (f(n_R) + g(n_R)) \quad (14)$$

where $f(n_R)$ and $g(n_R)$ can be described by

$$f(n_R) = -\frac{E(\ln \det(\mathbf{W}^H \mathbf{W}))}{\hat{n}_T \ln 2} \quad (15)$$

$$g(n_R) = -\frac{\ln \det(\Lambda_R)}{\hat{n}_T \ln 2} \quad (16)$$

Because $\mathbf{W}^H \mathbf{W}$ is wishart matrix and nonsingular with probability 1, $f(n_R)$ is reduced to [9]

$$\begin{aligned} f(n_R) &= -\frac{1}{\hat{n}_T \ln 2} E(\log_e \det(\mathbf{W}^H \mathbf{W})) \\ &= -\frac{1}{\hat{n}_T \ln 2} \sum_{l=0}^{\hat{n}_T-1} \psi(n_R - l) \end{aligned} \quad (17)$$

where $\psi(\cdot)$ is digamma function and the definition of digamma function is

$$\psi(n) = -\gamma + \sum_{l=1}^{n-1} \frac{1}{l} \quad (18)$$

where γ is Euler-Mascheroni constant, and

$$\gamma = \lim_{n \rightarrow \infty} \left(\sum_{l=1}^n \frac{1}{l} - \log_e n \right) \approx 0.5772 \quad (19)$$

When it comes to function $g(n_R)$, the derivation of $g(n_R)$ can be expressed as

$$g(n_R) = -\frac{1}{\hat{n}_T \ln 2} \ln \det(\Lambda_R) = -\frac{1}{\hat{n}_T \ln 2} \ln \det(\Sigma_R) \quad (20)$$

It can be found from (20) that $g(n_R)$ is only determined by the determinant of Σ_R , and the determinant of n_R order tri-diagonal toeplitz matrix Σ_R can be computed by [20].

$$\det \Sigma_R = \begin{cases} \frac{\left((1 + \sqrt{1 - 4\alpha^2})^{n_R+1} - (1 - \sqrt{1 - 4\alpha^2})^{n_R+1} \right)}{2^{n_R+1} \sqrt{1 - 4\alpha^2}} & (1 - 4\alpha^2 \neq 0) \\ \frac{n_R + 1}{2^{n_R}} & (1 - 4\alpha^2 = 0) \end{cases} \quad (21)$$

With the aid of numerical computation and mathematical analysis, the curve of the determinant of tri-diagonal toeplitz matrix can be fit by some tractable elementary

function. When $1-4\alpha^2 \neq 0$ in (21), $\det \mathbf{\Sigma}_R$ can be approximated by the fitted curve as follow:

$$h(n_R) = 1 - 5\alpha^2 = 1 - 5J_0\left(2\pi \frac{L_R}{n_R - 1}\right)^2 \quad (22)$$

The approximation between the fitted curves and determinant curves of tri-diagonal toeplitz matrix are illustrated in Figure 3 and Figure 4. From Figure 3 and 4, we can find that the fitting curve can exactly approach the extreme points of the determinant of tri-diagonal toeplitz matrix. However, the expression is much simpler. In other words, the further derivation using the fitted curve is tractable using well-known mathematical software such as WOLFRAM MATHEMATICA.

In the following context, power offset is analyzed in detail. The approximate analysis of power offset is based on the piecewise function of n_R . The condition $1-5\alpha^2 > 0$ in (22) is necessary due to $\det \mathbf{\Sigma}_R > 0$, so the number of receiver antenna n_R can not be large than $4L_R + 1$. Moreover, it shows from the conclusion in [21] that the effect of correlation can be neglected when the normalized length of receive antenna array L_R is larger than one wave length, that is to say $n_R > L_R + 1$. Hence, the considered range of the number of receive antenna is $L_R + 1 < n_R < 4L_R + 1$.

With the discussion above, when $n_R \leq L_R + 1$, the normalized length of receive antenna array L_R is large

than one wave length and the effect of correlation can be neglected, that is to say $g(n_R) = 0$ and the power offset is expressed as

$$L_\infty = \log_2 \widehat{n}_T - \frac{1}{\widehat{n}_T \ln 2} \sum_{l=0}^{\widehat{n}_T - 1} \psi(n_R - l) \quad (23)$$

When it comes to the range of $L_R + 1 < n_R < 4L_R + 1$, the normalized length of receive antenna array L_R is smaller than one wave length and the effect of correlation can not be neglected. In other words, $g(n_R) \neq 0$. However, for a given value of \widehat{n}_T , the first-order derivative ($f(n_R)$ is assumed to be continuous) of $f(n_R)$ is obtained by

$$\begin{aligned} \frac{df(n_R)}{dn_R} &= \left(-\frac{1}{\widehat{n}_T \ln 2} \sum_{l=0}^{\widehat{n}_T - 1} \psi(n_R - l) \right)' \\ &= -\frac{1}{\widehat{n}_T \ln 2} \sum_{l=0}^{\widehat{n}_T - 1} \psi_1(n_R - l) \approx 0 \end{aligned} \quad (24)$$

where $\psi_1(\cdot)$ is trigamma function. Hence, it shown from (24) that $f(n_R)$ approximately equal to the constant C (approximation accuracy is related to the value of \widehat{n}_T). The power offset is expressed as

$$L_\infty \approx \log_2 \widehat{n}_T + g(n_R) + C \quad (25)$$

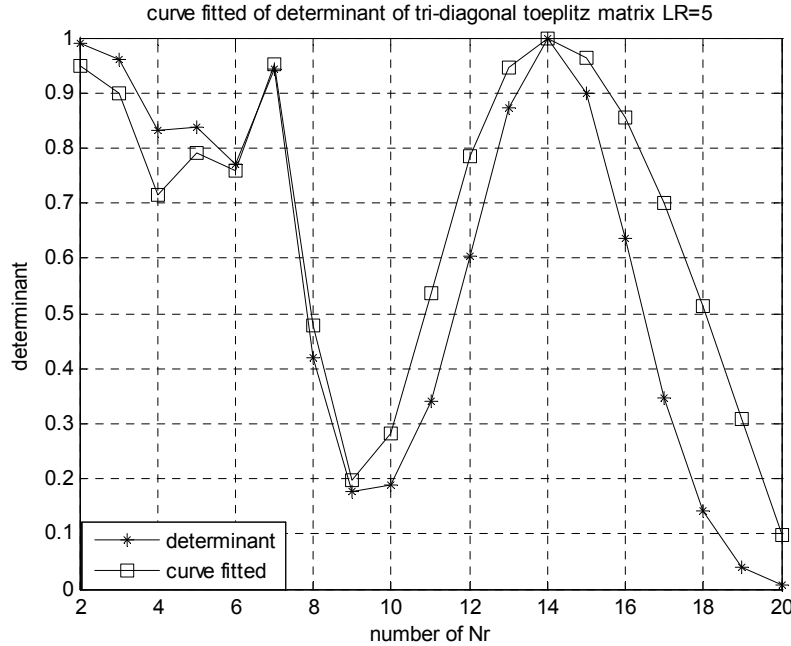


Figure 3. Approximation of determinant of tri-diagonal toeplitz matrix by curve fitting and $L_R = 5$

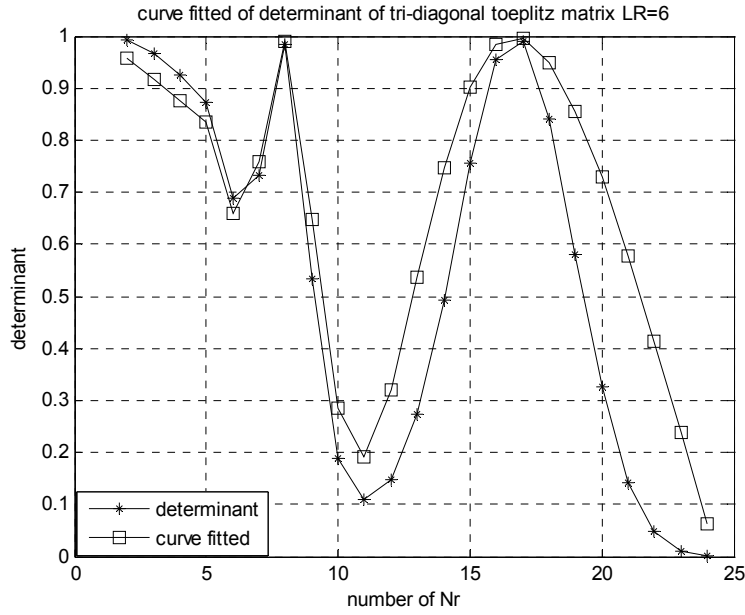


Figure 4. Approximation of determinant of tri-diagonal toeplitz matrix by curve fitting and $L_R = 6$

Without loss of generality, the constant C can be neglected in the approximate computation. Hence, the power offset in (25) is only determined by $g(n_R)$. From (22), the curve of the determinant of tri-diagonal toeplitz matrix can be fitted by $h(n_R) = 1 - 5\alpha^2$, where $\alpha = J_0\left(\frac{2\pi L_R}{n_R - 1}\right)$. The first order derivative ($h(n_R)$ is assumed to be continuous) of $h(n_R)$ can be computed by

$$\frac{dh(n_R)}{dn_R} = -\frac{4\pi L_R J_0\left(\frac{2\pi L_R}{n_R - 1}\right) J_1\left(\frac{2\pi L_R}{n_R - 1}\right)}{(n_R - 1)^2} \quad (26)$$

where $L_R + 1 < n_R < 4L_R + 1$, that is to say $\frac{\pi}{2} < \frac{2\pi L_R}{n_R - 1} < 2\pi$. In the range above, function

$J_0\left(\frac{2\pi L_R}{n_R - 1}\right)$ in (26) has two zero points, i.e.

$$P_1 = \frac{2\pi L_R}{n_R - 1} = 2.4048 \quad \text{and} \quad P_2 = \frac{2\pi L_R}{n_R - 1} = 5.5201, \quad \text{and}$$

function $J_1\left(\frac{2\pi L_R}{n_R - 1}\right)$ only has one zero point, i.e.

$$P_3 = \frac{2\pi L_R}{n_R - 1} = 3.8317. \quad \text{Consequently, } h(n_R) \text{ has three}$$

extreme points in the range of $\frac{\pi}{2} < \frac{2\pi L_R}{n_R - 1} < 2\pi$, described by P_i , $i = 1, 2, 3$.

And then, the second-order derivative of $h(n_R)$ can be computed by

$$\begin{aligned} \frac{d^2 h(n_R)}{dn_R^2} &= \frac{8\pi L_R J_0\left(\frac{2\pi L_R}{n_R - 1}\right) J_1\left(\frac{2\pi L_R}{n_R - 1}\right)}{(n_R - 1)^3} \\ &\quad - \frac{8\pi^2 L_R^2 J_1\left(\frac{2\pi L_R}{n_R - 1}\right)^2}{(n_R - 1)^4} \\ &\quad + \frac{4\pi^2 L_R^2 J_0\left(\frac{2\pi L_R}{n_R - 1}\right) \left[J_0\left(\frac{2\pi L_R}{n_R - 1}\right) - J_2\left(\frac{2\pi L_R}{n_R - 1}\right) \right]}{(n_R - 1)^4} \end{aligned} \quad (27)$$

Using (27), the second-order derivative in points P_i , $i = 1, 2, 3$ is obtained as follow:

$$P_1: \left. \frac{d^2 h(n)}{dn^2} \right|_{\frac{2\pi L_R}{n_R - 1} = 2.4048} = -\frac{4.51}{\pi^2 L_R^2} < 0 \quad (28)$$

$$P_2: \left. \frac{d^2 h(n)}{dn^2} \right|_{\frac{2\pi L_R}{n_R - 1} = 5.5201} = -\frac{53.75}{\pi^2 L_R^2} < 0 \quad (29)$$

$$P_3: \left. \frac{d^2 h(n)}{dn^2} \right|_{\frac{2\pi L_R}{n_R - 1} = 3.8317} = \frac{17.48}{\pi^2 L_R^2} > 0 \quad (30)$$

With the discussion above, it is obvious that point P_1 and P_2 are local maximum points of $h(n_R)$ and point

P_3 is local minimum point. Furthermore, it is obvious from (20) that the extreme points of $h(n_r)$ is same as ones of $g(n_r)$. Consequently, in the range of $L_R + 1 < n_r < 4L_R + 1$, the extreme points of power offset in (25) can be approximately computed by

$$\widehat{n}_R = \begin{cases} \arg \min_{n_r \in \Pi} (L_\infty), & \text{for local minimal point} \\ \arg \max_{n_r \in \Pi} (L_\infty), & \text{for local maximum point} \end{cases} \quad (31)$$

where Π is defined as follows:

$$\Pi = \left\{ \left\lfloor \frac{2\pi L_R}{P_i} + 1 \right\rfloor, \left\lceil \frac{2\pi L_R}{P_i} + 1 \right\rceil \right\}, i = 1, 2, 3 \quad (32)$$

where $\lfloor x \rfloor$ and $\lceil x \rceil$ denote the maximum integer smaller than x and minimum integer larger than x , respectively. P_i , $i = 1, 2, 3$ is the extreme points computed above. (31) can be used to approximately compute the number of receive antenna, in order to achieve the optimal power offset.

5. Simulation Results

In the Figure 1 and 2, with the assumption of $\widehat{n}_T = 2$, power offset is approximately analyzed based on tri-diagonal, five-diagonal, and seven-diagonal toeplitz versus the number of receive antenna, with $L_R = 5$ in Figure 1 and $L_R = 6$ in Figure 2. Furthermore, power offset in independent channel is also provided as lower bound for numerical comparison. The approximation trend can be

found from Figure 1 and 2. The tri-diagonal toeplitz matrix can be assumably used to characterize the property of power offset over spatially correlated channel. Hence, tri-diagonal toeplitz matrix can be used to approximate the correlation model at the receive node.

The approximation of fitting the curve of tri-diagonal toeplitz matrix determinant is illustrated in Figure 3 and Figure 4 to compare the difference between fitted curves and determinant curves, with $L_R = 5$ in Figure 3 and $L_R = 6$ in Figure 4. From Figure 3 and 4, we can find that the fitting curve can exactly approach the extreme points of the determinant of tri-diagonal toeplitz matrix. However, the expression is mathematically tractable.

With the same assumption of $\widehat{n}_T = 2$, approximation of power offset is shown in Figure 5 and 6, with $L_R = 5$ in Figure 5 and $L_R = 6$ in Figure 6. From Figure 5 and 6, we can find the position of two local minimal points and one local maximum point. With the condition of $L_R = 5$ and $\widehat{n}_T = 2$, the local extreme points computed by (31) is $n_R = 9$ for local maximum point and $n_R = 7, 15$ for local minimal points. With the condition of $L_R = 6$ and $\widehat{n}_T = 2$, the local extreme points computed by (31) is $n_R = 11$ for local maximum point and $n_R = 8, 16$ for local minimal points. The computation results based on (31) coincide with the illustration results in Figure 5 and 6. Hence, all the approximation in this paper is reasonable, including approximation of correlation model and approximation of determinant of tri-diagonal toeplitz matrix.

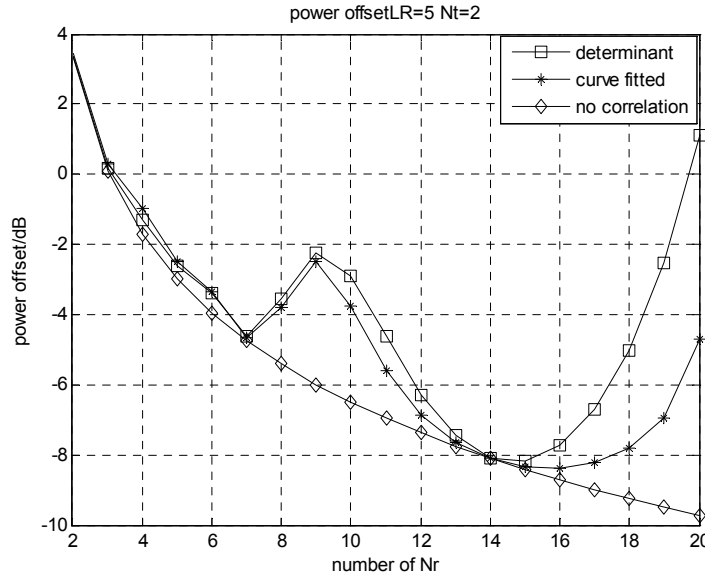


Figure 5. Power offset comparison between accurate and approximate determinant of toeplitz matrix with $L_R = 5$, $\widehat{n}_T = 2$

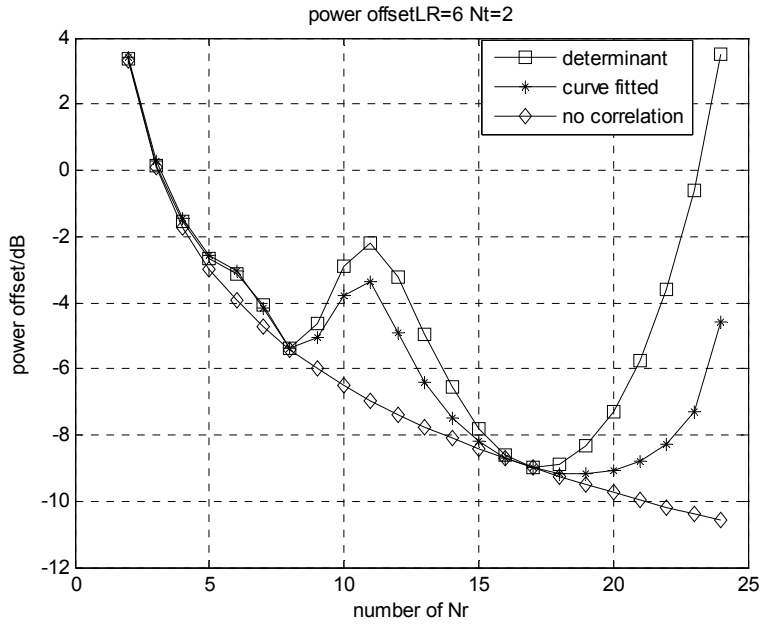


Figure 6. Power offset comparison between accurate and approximate determinant of toeplitz matrix with $L_R = 6$, $\hat{n}_T = 2$

Similar results are presented in Figure 7 and 8, with the assumption of $\hat{n}_T = 4$ and $L_R = 5$ in Figure 7 while $L_R = 8$ in Figure 8. With the condition of $L_R = 5$ and $\hat{n}_T = 4$, the local extreme points computed by (31) is $n_R = 9$ for local maximum point and $n_R = 7, 15$ for local minimal points. With the condition of $L_R = 8$ and $\hat{n}_T = 4$, the local extreme points computed by (31) is $n_R = 14$ for local maximum point and $n_R = 10, 22$ for

local minimal points. The computation results based on (31) coincide with the illustration results in Figure 7 and 8.

Consequently, it is presented in Figure 5 and 7 that the effect caused by the number \hat{n}_T can be neglected. In other words, for small value of \hat{n}_T and in the range of number of receive antenna $L_R + 1 < n_R < 4L_R + 1$, the assumption of $f(n_R) \approx C$ is tenable with neglectable loss of precision. The extreme points of power offset is only determined by $g(n_R)$.

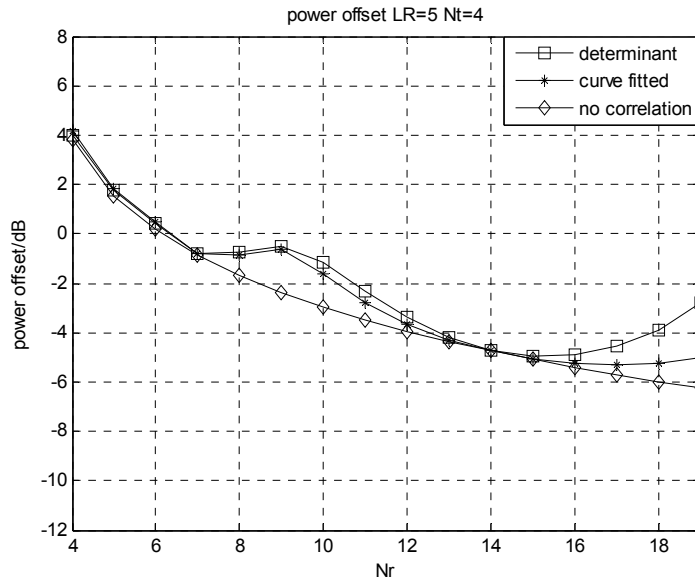


Figure 7. Power offset comparison between accurate and approximate determinant of toeplitz matrix with $L_R = 5$, $\hat{n}_T = 4$

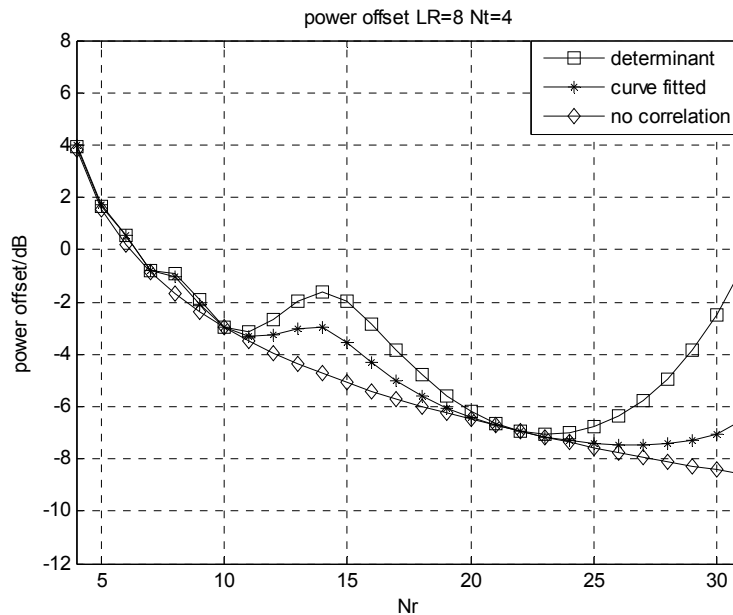


Figure 8. Power offset comparison between accurate and approximate determinant of toeplitz matrix with $L_R = 8$, $\hat{n}_r = 4$

6. Conclusions

Approximate analysis of power offset over spatially correlated channel is proposed to optimize the number of receive antenna with antenna array of fixed length. Antenna correlation matrix is approximated by tri-diagonal toeplitz matrix. The determinant of tri-diagonal toeplitz matrix is reduced to simple style by curve fitting with neglectable loss of precision. Based on the approximation above, the expression of local extreme points of power offset is derived. Simulation results shows that the derived expression is accurate in the local extreme points of power offset, that is to say, all the approximation in this paper is reasonable.

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